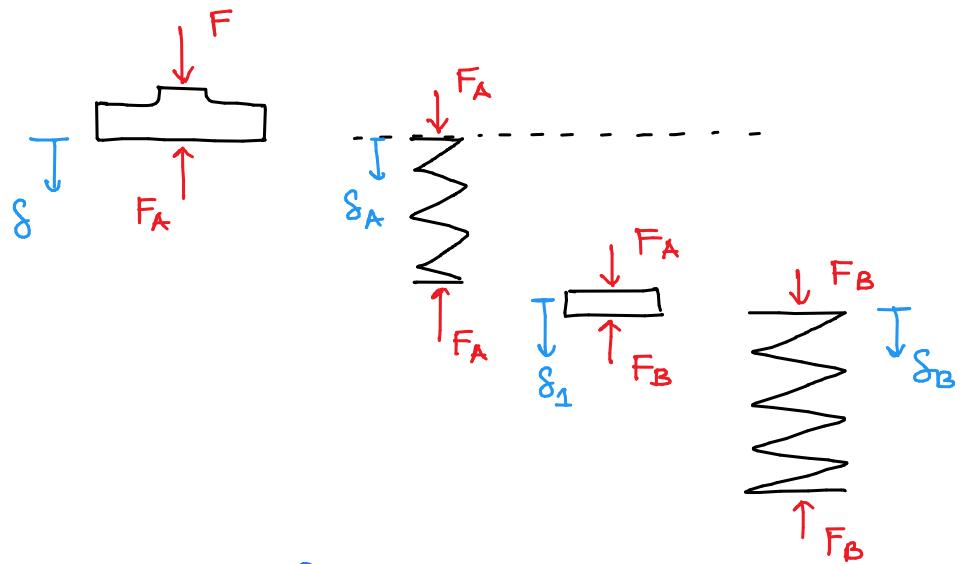


▷ Draw FBDs



Force equilibrium

Piston 1

$$+\uparrow \sum F_y = 0$$

$$\Rightarrow F_A - F = 0 \Rightarrow F_A = F \quad (1)$$

Piston 2

$$+\uparrow \sum F_y = 0$$

$$\Rightarrow F_B - F_A = 0 \Rightarrow F_B = F_A \quad (2)$$

Using ① & ②, $F_A = F_B = F$

Deformation and geometric compatibility

Compression of spring A

$$\delta_A = \delta - \delta_1 \quad (3)$$

Compression of spring B

$$\delta_B = \delta_1 \quad (4)$$

Using ③ & ④, $\delta = \delta_A + \delta_B$

Force-deformation relations

Spring A

$$\delta_A = F/k_A \quad (5)$$

Spring B

$$\delta_B = F/k_B \quad (6)$$

$$\text{So, } \delta = F \left(\frac{1}{k_A} + \frac{1}{k_B} \right) \Rightarrow F = \frac{1}{\left(\frac{1}{k_A} + \frac{1}{k_B} \right)}$$

effective stiffness

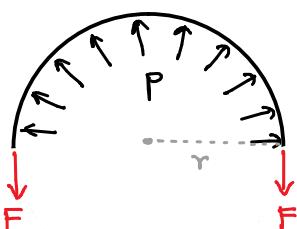
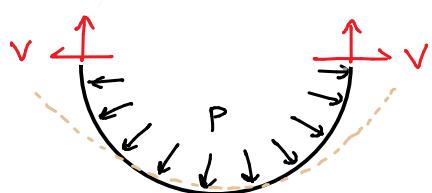
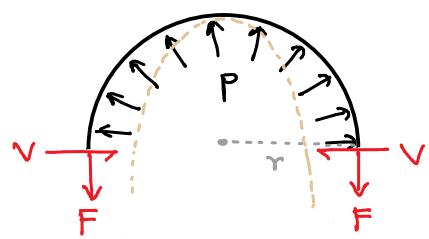
$$\delta = \underbrace{\left(\frac{k_A k_B}{k_A + k_B} \right)}_{\text{effective stiffness}} \delta$$

$$\delta_B = F/k_B \Rightarrow \delta_B = \left(\frac{k_A}{k_A + k_B} \right) \delta$$

Similarly, find δ_A

2) See Example 2.3(a) of Crandall & Dahl book

3) Let's draw an FBD of the ring by cutting a section through its diameter



- Due to Newton's 3rd law the shear forces must act equally and oppositely on the two halves
- For the top half the shear forces V has a tendency to push the ring inside, while those on the lower half tends to push it outside
- To maintain continuity and symmetry, the shear forces V must be equal to ZERO

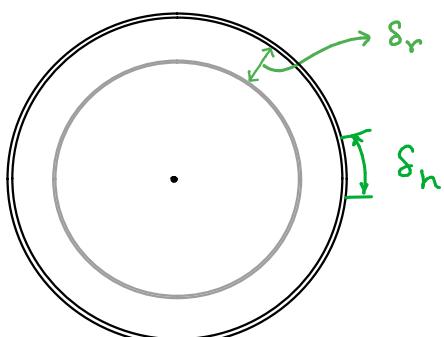
The effective vertical force due to the internal pressure $= (p_b)(2r) = 2pbr$

This force is resisted by $2F$

From force equilibrium in vertical direction, we get:

$$F = pbr$$

Deformation and Geometric Compatibility



Let the increase in the circumference of ring be δ_h and the deformation in the radial direction be δ_r

The increase in circumference is accompanied by a radial expansion $\delta_r = \delta_h / 2\pi$

Force-deformation relation

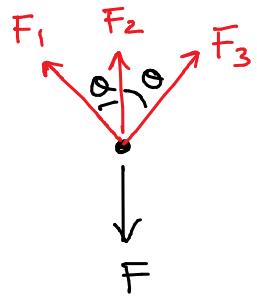
Increase in circumference of ring

$$\begin{aligned}\delta_h &= \frac{F L}{A E} = \frac{(P b r) (2\pi(r + \frac{t}{2}))}{(t b) E} \quad \therefore \delta_r = \frac{Pr^2}{t E} \left(1 + \frac{t}{2r}\right) \\ &= \frac{2\pi P r^2}{t E} \left(1 + \frac{t}{2r}\right)\end{aligned}$$

Thin ring assumption $t \ll r$, then $\frac{t}{r} \ll 1$

$$\delta_h = \frac{2\pi P r^2}{t E}, \quad \delta_r = \frac{Pr^2}{t E}$$

4>



Force equilibrium

$$\rightarrow \sum F_x = 0$$

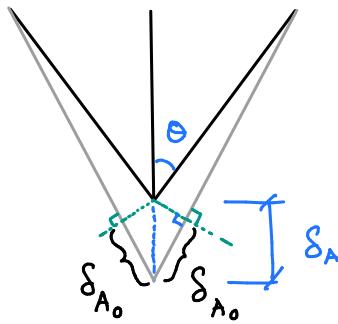
$$\Rightarrow -F_1 \sin \theta + F_3 \sin \theta = 0$$

$$\Rightarrow F_1 = F_3$$

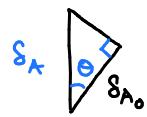
$$\rightarrow \sum F_y = 0$$

$$\Rightarrow 2F_1 \cos \theta + F_2 = F$$

Deformation & Geometric compatibility



Due to the symmetry of the system, there would only be vertical deformation δ_A at the free end



From small deformation, we can utilize geometric compatibility as

$$\delta_{A_0} = \delta_A \cos \theta$$

Force-deformation relation

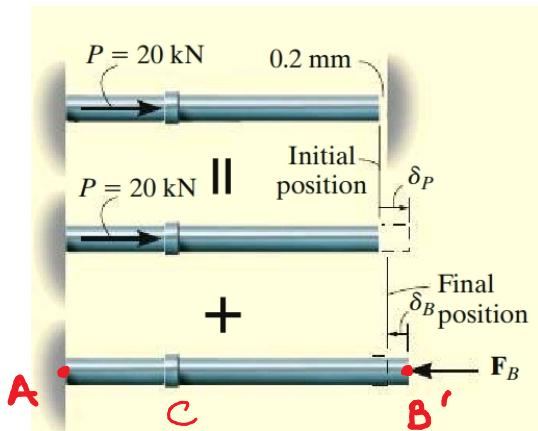
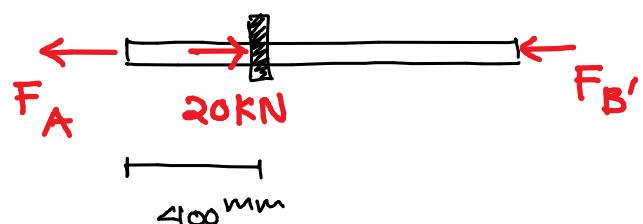
$$\frac{F_1 (\cancel{L}/\cos \theta)}{A_0 \cancel{E}} = \frac{F_2 \cancel{L}}{A \cancel{E}} \cos \theta$$

$$\Rightarrow F_1 = F_2 \left(\frac{A_0}{A} \right) \cos^2 \theta$$

Therefore, $2F_2 \left(\frac{A_0}{A} \right) \cos^3 \theta + F_2 = F \Rightarrow F_2 = \frac{F}{\left(1 + 2 \frac{A_0}{A} \cos^3 \theta \right)}$

and $F_1 = \frac{F}{\left(\frac{A}{A_0 \cos^2 \theta} + 2 \cos \theta \right)}$

5>

FBD

Force equilibrium

$$\stackrel{+}{\rightarrow} \sum F_x = 0 \Rightarrow F_A + F_B - 20 = 0 \rightarrow F_A = 15.95 \text{ kN}$$

Deformation & Compatibility

If there was no support at B', then the displacement would have been $\delta_p = \frac{PL_{AC}}{AE}$

$$\begin{aligned}\delta_p &= \frac{(20 \times 10^3 \text{ N})(0.4 \text{ m})}{(\pi \times 0.005^2 \text{ m}^2)(200 \times 10^9 \text{ N/m}^2)} \\ &= 0.5093 \times 10^{-3} \text{ m}\end{aligned}$$

Due to the load F_B' , acting on the right hand wall, the portion CB' would be compressed by amount say δ_B

From compatibility, it must be that

$$\begin{aligned}\delta_p - \delta_B &= 0.2 \times 10^{-3} \text{ m} \\ \Rightarrow \delta_B &= 0.3093 \times 10^{-3} \text{ m}\end{aligned}$$

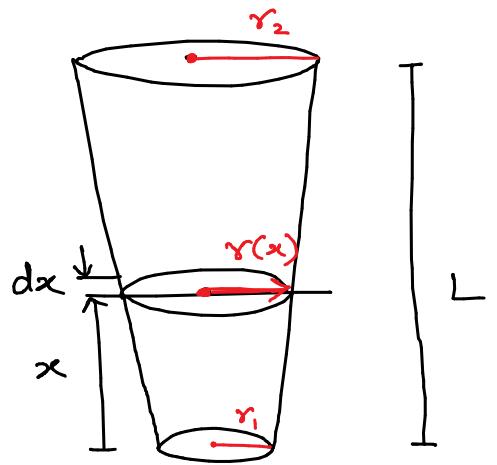
Force-deformation relation

$$\delta_B = \frac{F_B L_{AB}}{AE} \Rightarrow F_B = \frac{(\pi \times 0.005 \text{ m}^2)(200 \times 10^9 \text{ N/m}^2)}{(1.2002 \text{ m})} \delta_B$$

$$\delta_B = 4.05 \text{ kN}$$

$$6) \quad r(x) = r_1 + \left(\frac{r_2 - r_1}{L} \right) x \\ = \frac{r_1 L + (r_2 - r_1)x}{L}$$

$$A(x) = \frac{\pi}{L^2} (r_1 L + (r_2 - r_1)x)^2$$



$$\begin{aligned} S &= \int_0^L \frac{P \, dx}{A(x) E} = \frac{P L^2}{\pi E} \int_0^L \frac{dx}{[r_1 L + (r_2 - r_1)x]^2} \\ &= -\frac{PL^2}{\pi E} \left[\frac{1}{(r_2 - r_1)[r_1 L + (r_2 - r_1)x]} \right] \Big|_0^L \\ &= -\frac{PL^2}{\pi E (r_2 - r_1)} \left[\frac{1}{r_2 L} - \frac{1}{r_1 L} \right] \\ &= \cancel{-\frac{PL^2}{\pi E (r_2 - r_1)}} \left[\frac{\cancel{r_1} - \cancel{r_2}}{r_1 r_2 L} \right] \\ &= \frac{PL}{\pi E r_1 r_2} \end{aligned}$$