

## Tutorial 6 (Part A)

A thin homogeneous rectangular plate, as shown, rotates about a diagonal axis with angular velocity  $\underline{\omega}$  and angular acceleration  $\dot{\underline{\omega}}$ .

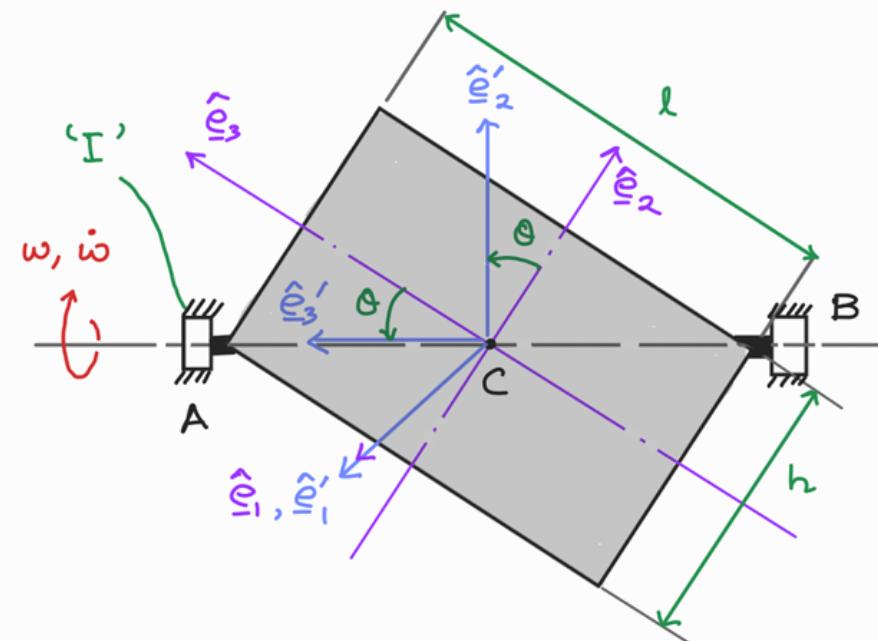
- (i) Determine the total moment  $M_C$  exerted on the plate about the COM  $C$ , ~~using~~ the coordinate system  $\hat{e}'_1, \hat{e}'_2, \hat{e}'_3$  in terms of the rotational motion  $\underline{\omega}$  and  $\dot{\underline{\omega}}$ .
- (ii) Find the relation between a drive torque  $\underline{T} = T\hat{e}'_3$  (applied about  $\hat{e}'_3$ -axis) to the rotational motion. Also, determine the bearing support reaction forces (assuming bearing support reaction couples are zero).

Given:  $\underline{\omega}_{m|I} = \omega \hat{e}'_3$

$$\dot{\underline{\omega}}_{m|I} = \dot{\omega} \hat{e}'_3$$

plate lies in the plane of  
 $x_2(\hat{e}_3) - x_3(\hat{e}_3) / x'_2(\hat{e}'_3) - x'_3(\hat{e}'_3)$

Both CSys are body-fixed.



Solution: RB 'm' ← rectangular plate rotates about an axis

We can make use of the simplified Euler's 2nd equation for an RB rotating about a fixed axis.

Recall the simplified Euler's 2nd equation at point A of the RB rotating about a fixed body axis  $\hat{e}_3$

$$\underline{M}_A = \underbrace{\left( I_{13}^A \dot{\omega} - I_{23}^A \omega^2 \right)}_{M_{A,1}} \hat{e}_1 + \underbrace{\left( I_{23}^A \dot{\omega} + I_{13}^A \omega^2 \right)}_{M_{A,2}} \hat{e}_2 + \underbrace{I_{33}^A \dot{\omega}}_{M_{A,3}} \hat{e}_3$$

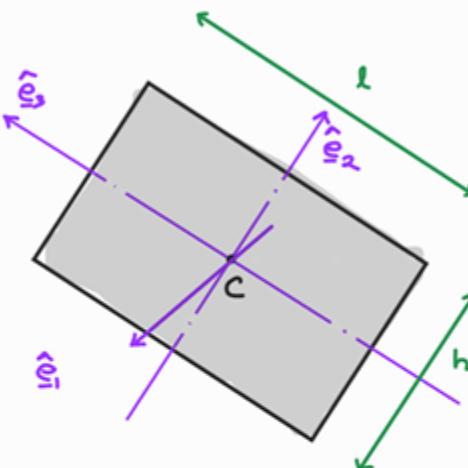
With the body-fixed csys being  $\hat{\underline{e}}_1' - \hat{\underline{e}}_2' - \hat{\underline{e}}_3'$ , we rewrite

the equation as:  $A \equiv C$ ,  $\hat{\underline{e}}_i \rightarrow \hat{\underline{e}}_i'$

$$\underline{M}_C = \underbrace{\left( I_{13}^C \dot{\omega} - I_{23}^C \omega^2 \right)}_{M_{C,1}'} \hat{\underline{e}}_1' + \underbrace{\left( I_{23}^C \dot{\omega} + I_{13}^C \omega^2 \right)}_{M_{C,2}'} \hat{\underline{e}}_2' + \underbrace{I_{33}^C \dot{\omega}}_{M_{C,3}'} \hat{\underline{e}}_3'$$

To determine  $\underline{M}_C$ , we need to calculate the inertia matrix components in  $\hat{\underline{e}}_1' - \hat{\underline{e}}_2' - \hat{\underline{e}}_3$  csys.

Note:  $\hat{\underline{e}}_1 - \hat{\underline{e}}_2 - \hat{\underline{e}}_3$  csys coincide with the principal axes of inertia of the rectangular plate (due to planes of symmetry)



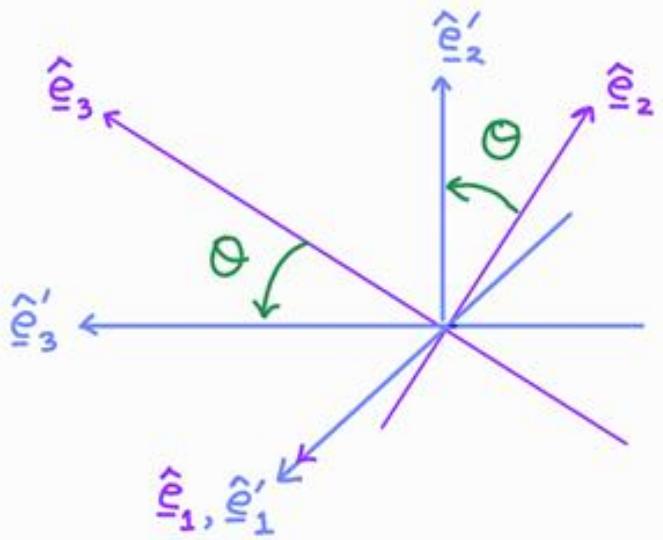
$$\Rightarrow \begin{bmatrix} \underline{\underline{I}}^c \end{bmatrix} \begin{pmatrix} \hat{\underline{e}}_1 \\ \hat{\underline{e}}_2 \\ \hat{\underline{e}}_3 \end{pmatrix} = \begin{bmatrix} I_{11}^c & 0 & 0 \\ 0 & I_{22}^c & 0 \\ 0 & 0 & I_{33}^c \end{bmatrix} = \begin{bmatrix} \frac{m(l^2+h^2)}{12} & 0 & 0 \\ 0 & \frac{ml^2}{12} & 0 \\ 0 & 0 & \frac{mh^2}{12} \end{bmatrix}$$

Next we will use inertia matrix transformation law

to find the components of  $\underline{\underline{I}}^c$  in  $\hat{\underline{e}}'_1 - \hat{\underline{e}}'_2 - \hat{\underline{e}}'_3$  csys

$$[\underline{\underline{I}}^c] \begin{pmatrix} \hat{\underline{e}}_1' \\ \hat{\underline{e}}_2' \\ \hat{\underline{e}}_3' \end{pmatrix} = [\underline{\underline{A}}] [\underline{\underline{I}}_c] \begin{pmatrix} \hat{\underline{e}}_1 \\ \hat{\underline{e}}_2 \\ \hat{\underline{e}}_3 \end{pmatrix} [\underline{\underline{A}}]^T$$

Find transformation matrix  $[\underline{\underline{A}}]$  : Use  $A_{ij} = \hat{\underline{e}}_i' \cdot \hat{\underline{e}}_j$



$$A_{22} = \hat{\underline{e}}_2' \cdot \hat{\underline{e}}_2 = \cos\theta = c$$

$$A_{23} = \hat{\underline{e}}_2' \cdot \hat{\underline{e}}_3 = \sin\theta = s$$

$$A_{32} = \hat{\underline{e}}_3' \cdot \hat{\underline{e}}_2 = -\sin\theta = -s$$

$$A_{33} = \hat{\underline{e}}_3' \cdot \hat{\underline{e}}_3 = \cos\theta = c$$

$$A_{11} = 1, \quad A_{21} = A_{31} = 0$$

$$\begin{aligned}
 [\underline{\underline{I}}^c] \begin{pmatrix} \hat{e}_1' \\ \hat{e}_2' \\ \hat{e}_3' \end{pmatrix} &= \begin{bmatrix} 1 & 0 & 0 \\ 0 & c & s \\ 0 & -s & c \end{bmatrix} \begin{bmatrix} I_{11}^c & 0 & 0 \\ 0 & I_{22}^c & 0 \\ 0 & 0 & I_{33}^c \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 \\ 0 & c & s \\ 0 & -s & c \end{bmatrix}^T \\
 &= \begin{bmatrix} I_{11}^c & 0 & 0 \\ 0 & c^2 I_{22}^c + s^2 I_{33}^c & cs(-I_{22}^c + I_{33}^c) \\ 0 & sym & s^2 I_{22}^c + c^2 I_{33}^c \end{bmatrix}
 \end{aligned}$$

From geometry of plate :  $\sin \theta = \frac{h}{\sqrt{l^2+h^2}}$ ,  $\cos \theta = \frac{l}{\sqrt{l^2+h^2}}$

Given :  $[\underline{\omega}] \begin{pmatrix} \hat{e}_1' \\ \hat{e}_2' \\ \hat{e}_3' \end{pmatrix} = \begin{bmatrix} 0 \\ 0 \\ \omega \end{bmatrix}$  &  $[\dot{\underline{\omega}}] \begin{pmatrix} \hat{e}_1' \\ \hat{e}_2' \\ \hat{e}_3' \end{pmatrix} = \begin{bmatrix} 0 \\ 0 \\ \dot{\omega} \end{bmatrix} = 0$

Let's now use simplified Euler's 2nd equation:

$$\underline{M}_c = \underbrace{\left( I_{13}^c \dot{\omega} - I_{23}^c \omega^2 \right) \hat{e}_1' }_{M'_{c,1}} + \underbrace{\left( I_{23}^c \dot{\omega} + I_{13}^c \omega^2 \right) \hat{e}_2' }_{M'_{c,2}} + \underbrace{I_{33}^c \dot{\omega} \hat{e}_3'}_{M'_{c,3}}$$

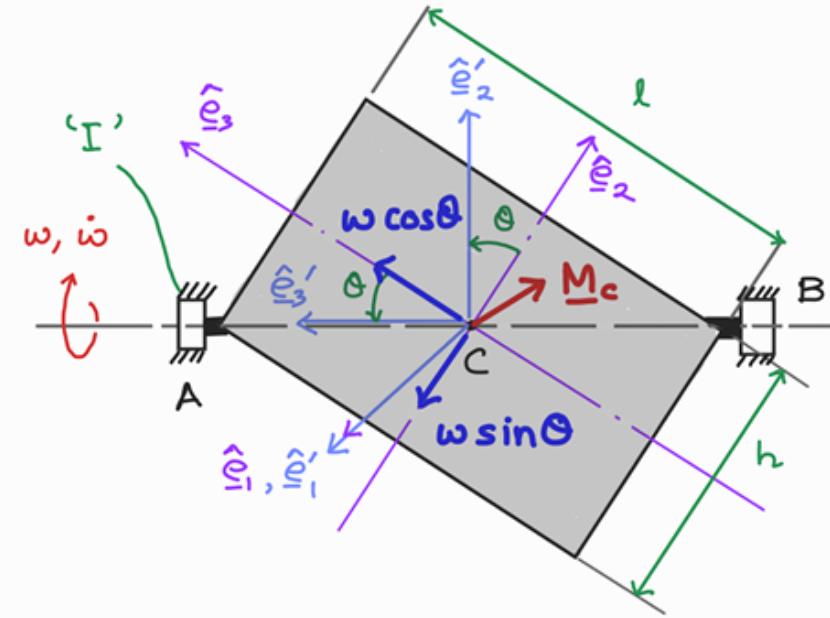
$$\begin{aligned}
 M'_{c,1} &= -\frac{1}{12} m (-l^2 + h^2) \sin\Theta \cos\Theta \omega^2 \\
 &= -\frac{m l h}{12} \frac{(-l^2 + h^2)}{(l^2 + h^2)} \omega^2 \\
 M'_{c,2} &= \frac{m l h}{12} \frac{(-l^2 + h^2)}{(l^2 + h^2)} \dot{\omega} \\
 M'_{c,3} &= \left( \sin^2\Theta \frac{m l^2}{12} + \cos^2\Theta \frac{m h^2}{12} \right) \dot{\omega} \\
 &= \frac{m}{12} \left( \frac{h^2 l^2}{l^2 + h^2} + \frac{l^2 h^2}{l^2 + h^2} \right) \dot{\omega} \\
 &= \frac{m h^2 l^2}{6(l^2 + h^2)} \dot{\omega}
 \end{aligned}
 \quad \left. \right\} \textcircled{*}$$

Alternative way : Using simplified Euler's 2nd equation

in csys  $\hat{\underline{e}}_1 - \hat{\underline{e}}_2 - \hat{\underline{e}}_3$  (coinciding with p-axes of plate)

Let's solve the problem  
using p-axes csys!

$$[\underline{\omega}] \begin{pmatrix} \hat{\underline{e}}_1 \\ \hat{\underline{e}}_2 \\ \hat{\underline{e}}_3 \end{pmatrix} = \begin{bmatrix} 0 \\ -\omega \sin \theta \\ \omega \cos \theta \end{bmatrix}$$



$$[\dot{\underline{\omega}}] \begin{pmatrix} \hat{\underline{e}}_1 \\ \hat{\underline{e}}_2 \\ \hat{\underline{e}}_3 \end{pmatrix} = \begin{bmatrix} 0 \\ -\dot{\omega} \sin \theta \\ \dot{\omega} \cos \theta \end{bmatrix}$$

where  $\sin \theta = \frac{h}{\sqrt{l^2 + h^2}} \equiv s$

$\cos \theta = \frac{l}{\sqrt{l^2 + h^2}} \equiv c$

Since  $\hat{e}_1 - \hat{e}_2 - \hat{e}_3$  coincides with p-axes of inertia of the rectangular plate

$$[\underline{\underline{I}}^c] \begin{pmatrix} \hat{e}_1 \\ \hat{e}_2 \\ \hat{e}_3 \end{pmatrix} = \begin{bmatrix} \frac{m(l^2+h^2)}{12} & 0 & 0 \\ 0 & \frac{ml^2}{12} & 0 \\ 0 & 0 & \frac{mh^2}{12} \end{bmatrix}$$

Now let's use simplified Euler's 2nd equation at pt C

in the  $\hat{e}_1 - \hat{e}_2 - \hat{e}_3$  csys (coinciding with p-axes of RB at C)

$$\underline{M}_c = M_{c,1} \hat{\underline{e}}_1 + M_{c,2} \hat{\underline{e}}_2 + M_{c,3} \hat{\underline{e}}_3$$

$$\underline{M}_c = \left[ I_{11}^c \cancel{\dot{\omega}_1^o} - (I_{22}^c - I_{33}^c) \omega_2 \omega_3 \right] \hat{\underline{e}}_1$$

$$+ \left[ I_{22}^c \cancel{\dot{\omega}_2^o} - (I_{33}^c - I_{11}^c) \omega_3 \cancel{\dot{\omega}_1^o} \right] \hat{\underline{e}}_2$$

$$+ \left[ I_{33}^c \cancel{\dot{\omega}_3^o} - (I_{11}^c - I_{22}^c) \cancel{\dot{\omega}_1^o} \omega_2 \right] \hat{\underline{e}}_3$$

$$= - \underbrace{\frac{m \cancel{cs}}{12} (l^2 - h^2)}_{M_{c,1}} \omega^2 \hat{\underline{e}}_1 + \underbrace{\frac{m}{12} (-s l^2 \hat{\underline{e}}_2 + c h^2 \hat{\underline{e}}_3)}_{M_{c,2}} \cancel{\dot{\omega}}$$

$$+ \underbrace{\cancel{\frac{m}{12} (s l^2 \hat{\underline{e}}_2 + c h^2 \hat{\underline{e}}_3) \dot{\omega}}}_{M_{c,3}}$$

Note that  $M_{c,1}$ ,  $M_{c,2}$ , and  $M_{c,3}$  are components of  $\underline{M}_c$  in the  $\hat{\underline{e}}_1 - \hat{\underline{e}}_2 - \hat{\underline{e}}_3$  csys.

To get the components of  $\underline{M}_c$  in  $\hat{\underline{e}}_1' - \hat{\underline{e}}_2' - \hat{\underline{e}}_3'$  csys, one needs to use a transformation of coordinate sys :

$$[\underline{M}_c] \begin{pmatrix} \hat{\underline{e}}_1' \\ \hat{\underline{e}}_2' \\ \hat{\underline{e}}_3' \end{pmatrix} = [\underline{A}] [\underline{M}_c] \begin{pmatrix} \hat{\underline{e}}_1 \\ \hat{\underline{e}}_2 \\ \hat{\underline{e}}_3 \end{pmatrix}$$

$$\Rightarrow \begin{bmatrix} M_{c,1}' \\ M_{c,2}' \\ M_{c,3}' \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & c & s \\ 0 & -s & c \end{bmatrix} \begin{bmatrix} M_{c,1} \\ M_{c,2} \\ M_{c,3} \end{bmatrix}$$

$$\therefore M_{c,1}' = M_{c,1} = -\frac{m \ell h}{12} \frac{(-\ell^2 + h^2)}{(\ell^2 + h^2)} \omega^2$$

$$\begin{aligned}
 M_{c,2}' &= c M_{c,2} + s M_{c,3} \\
 &= \frac{m}{12} cs (-l^2 + h^2) \dot{\omega} \\
 &= \frac{m}{12} lh \frac{(-l^2 + h^2)}{(l^2 + h^2)} \dot{\omega}
 \end{aligned}$$

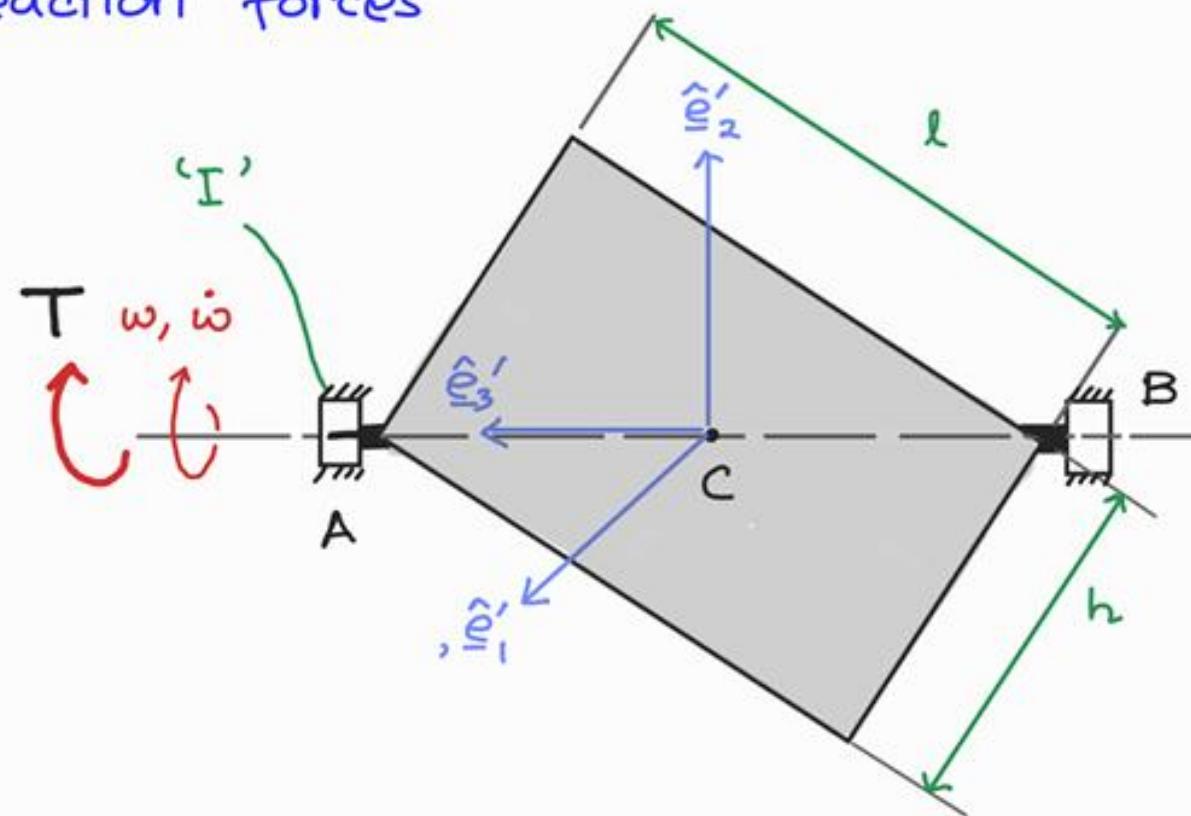
$$\begin{aligned}
 M_{c,3}' &= -s M_{c,2} + c M_{c,3} \\
 &= \frac{m}{12} (s^2 l^2 + c^2 h^2) \dot{\omega} = \frac{m h^2 l^2}{6(l^2 + h^2)} \dot{\omega}
 \end{aligned}$$

These are the same components we obtained using the 1st method.

Note that even if  $\dot{\omega}=0$ , still  $M_c \neq 0$  for a rotational motion with constant angular velocity  $\omega$ .

ii> Equation relating drive torque  $T$  to the rotation and dynamic bearing reaction forces

$$I = T \hat{e}'_3$$



Draw the FBD

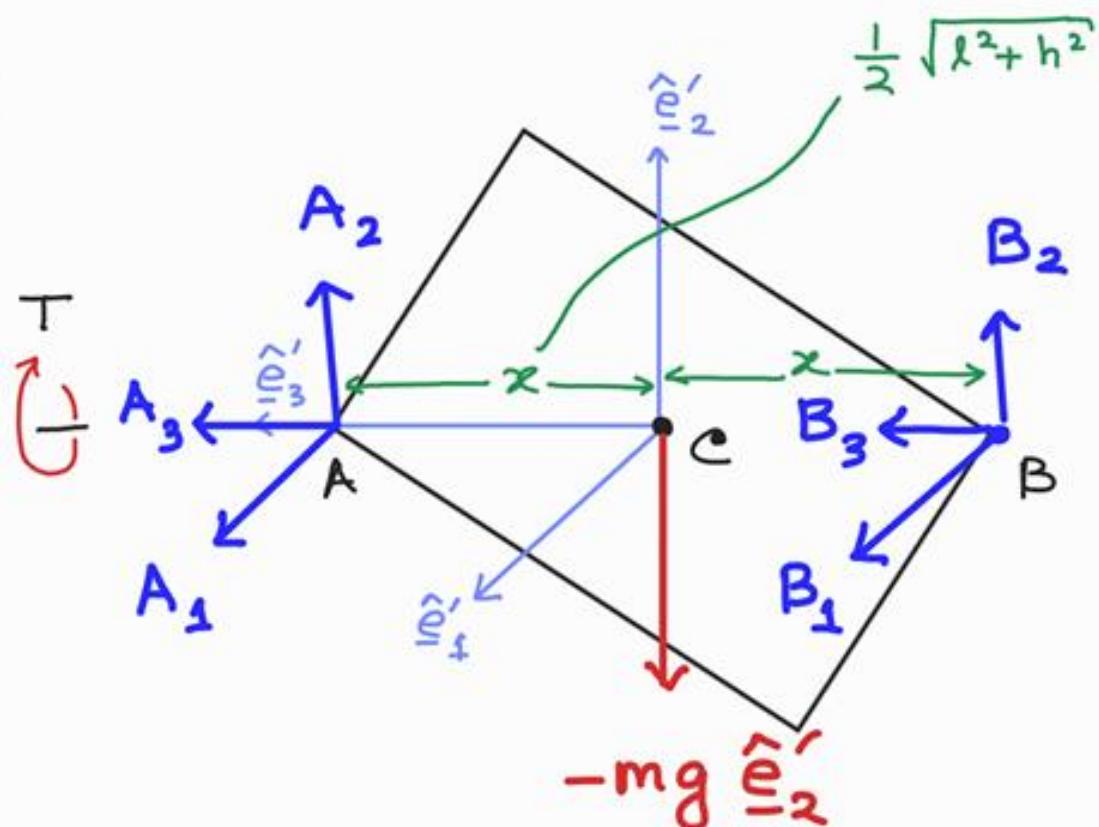
FBD

Assume zero reaction couples  
at supports (Given)

Reaction forces at  
supports A and B

$$A = A_1 \hat{e}_1' + A_2 \hat{e}_2' + A_3 \hat{e}_3'$$

$$B = B_1 \hat{e}_1' + B_2 \hat{e}_2' + B_3 \hat{e}_3'$$



From Euler's 1st eqn:

$$\underline{A} + \underline{B} - mg \hat{\underline{e}}_2' = m \underline{\alpha}_{clI}^0 = 0$$

$$\Rightarrow \underline{A} + \underline{B} = mg \hat{\underline{e}}_2$$

because C is  
on the  $\hat{\underline{e}}_3'$ -axis  
itself at all times!

Component-wise :  $B_1 = -A_1$

$$A_2 + B_2 = mg$$

$$B_3 = -A_3$$

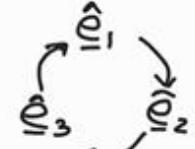
Express  $\underline{M}_c$  in terms of the external force system

$$\underline{M}_c = \underline{I} + \underline{r}_{AC} \times \underline{A} + \underline{r}_{BC} \times \underline{B}$$

( $-mg \hat{\underline{e}}_2'$  passes  
through C)

$$= T \hat{\underline{e}}_3' + (\cancel{x} \hat{\underline{e}}_3') \times (A_1 \hat{\underline{e}}_1' + A_2 \hat{\underline{e}}_2' + A_3 \hat{\underline{e}}_3')$$

$$+ (-\cancel{x} \hat{\underline{e}}_3') \times (B_1 \hat{\underline{e}}_1' + B_2 \hat{\underline{e}}_2' + B_3 \hat{\underline{e}}_3')$$



$$\begin{aligned}
 &= T \hat{\underline{e}}'_3 + A_1 x \hat{\underline{e}}'_2 - A_2 x \hat{\underline{e}}'_1 + A_1 x \hat{\underline{e}}'_2 + B_2 x \hat{\underline{e}}'_1 \\
 &= (\underbrace{-A_2 + B_2}_{} x \hat{\underline{e}}'_1 + \underbrace{A_1 (Qx)}_{=} \hat{\underline{e}}'_2 + \underbrace{T \hat{\underline{e}}'_3}_{=} \\
 &\quad = M_{c,1} \qquad \qquad \qquad = M_{c,2} \qquad \qquad \qquad = M_{c,3}
 \end{aligned}$$

Comparing these relations with the values obtained in  $\otimes$

$$\Rightarrow T = \frac{m h^2 l^2}{6(l^2 + h^2)} \dot{\omega}, \quad A_1 = -B_1 = -\frac{m l h}{12} \frac{(-l^2 + h^2)}{(l^2 + h^2)^{3/2}} \omega^2$$

and, finally  $A_2 + B_2 = mg$

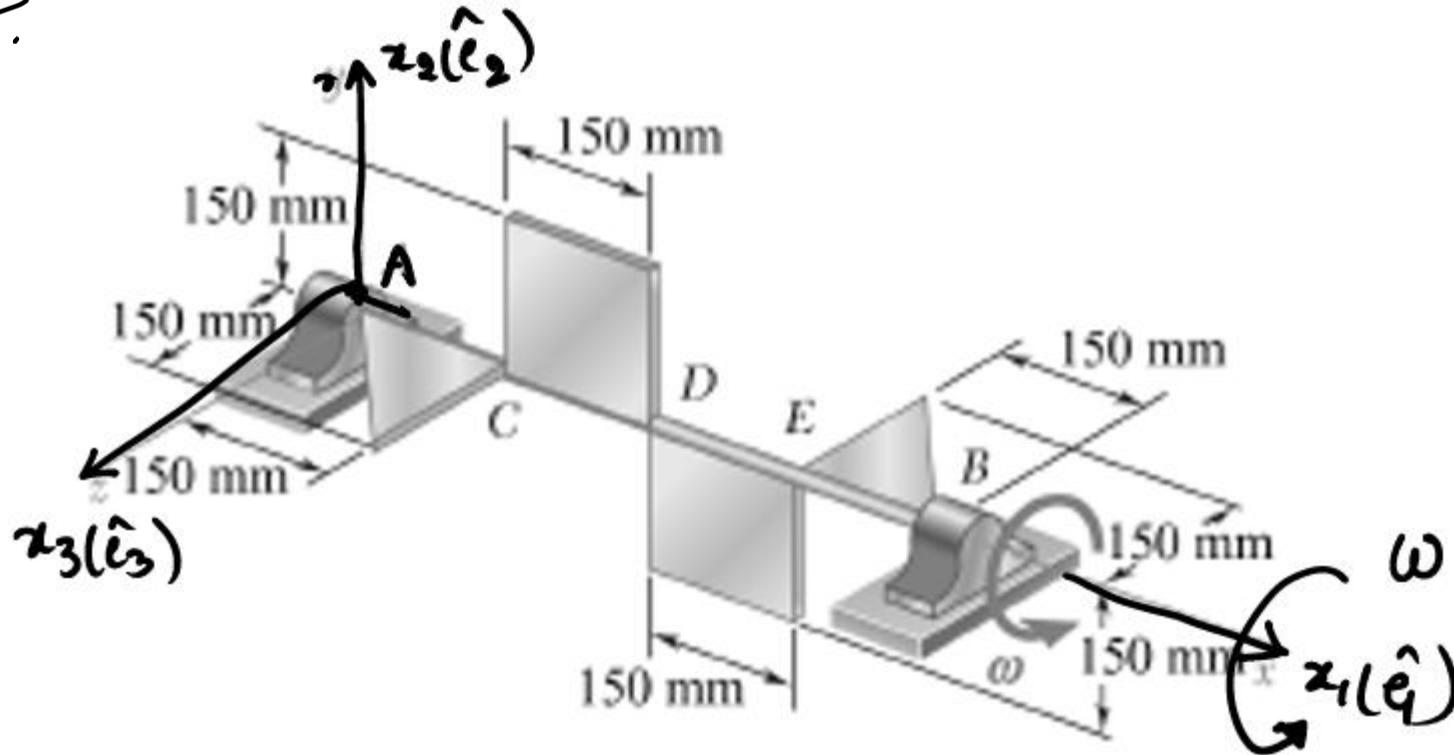
$$A_2 - B_2 = \frac{m l h}{24} \frac{(-l^2 + h^2)}{(l^2 + h^2)^{3/2}} \dot{\omega}$$

Solve  
to get  
values of  
 $A_2$  &  $B_2$

The axial reaction force components along  $\hat{\underline{e}}'_3$ ,  $A_3$  &  $B_3$   
cannot be determined from this analysis.

Q1. ... relate the reaction forces and moments of couples at A and B to the motion of the shaft. Angular velocity of the shaft is constant.

Set 6 B



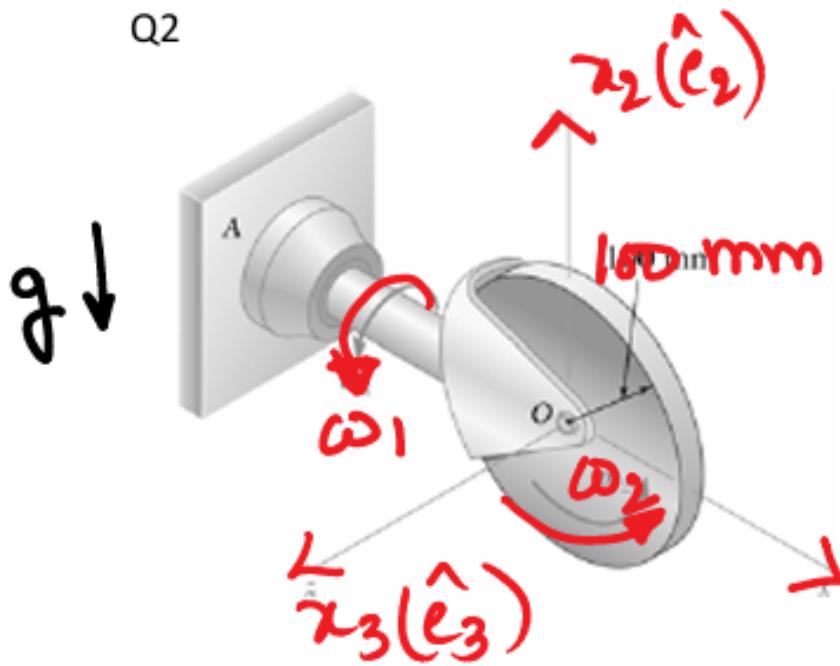
Answer:  $A_1 + B_1 = 0$ ,  $A_2 + B_2 = mg$ ,  $A_3 + B_3 = 0$

$$0.3A_3 - 0.3B_3 + C_{A2} + C_{B2} = -I_{31}^D \omega^2$$

$$-0.3A_2 + 0.3B_2 + C_{A3} + C_{B3} = I_{21}^D \omega^2$$

Set 6B: Q2

(Type II: problem)



PROBLEM 18.83 (Beck Johnston)

The uniform thin 2.5-kg disk spins at a constant rate  $\omega_2 = 6 \text{ rad/s}$  about an axis held by a housing attached to a horizontal rod that rotates at the constant rate  $\omega_1 = 3 \text{ rad/s}$ . ~~Determine the couple which presents the dynamic reaction at the support.~~ Find the force and moment of couple acting on the rod at A. (AO is massless)

$$\underline{F} = 1 \text{ N} \quad (\text{at this instant})$$

$$\underline{F} = 24.5 \text{ N vertically up}$$

$$\underline{C} = -0.225 \text{ N m} \hat{e}_2 + 24.5 \text{ N m} \hat{e}_3$$

$\Omega \hat{e}_1 \hat{e}_2 \hat{e}_3$  is fixed to the disk.